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THE FRENCH AEROSPACE LAB

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1st AIAA CFD Transition Modeling and Prediction Workshop

Case 4 – CRM-NLF – alpha sweep

Greg Delattre

Outline

- Solver & models
- Grids
- Pressure coefficient, transition lines
- Force and moment data
- Perspectives

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- **Solver & models**
- Grids
- Pressure coefficient, transition lines
- Force and moment data
- Perspectives

Solver & models

- elsA CFD solver © Airbus-Safran-Onera
- RANS FV on structured grids, 2nd order Roe scheme
- Menter SST turbulence model (SST-V on TMR)
- Transported AHD-GL transition model
 - Focusing on wing suction side
 - Transition is imposed
 - @ 5% x/c on wing pressure side
 - @ trip dots locations on fuselage nose

Stability-Based Transition Model using Transport Equations

<https://doi.org/10.2514/1.J058906>

- Combination of two transition criteria on Re_θ :
 - AHD \rightarrow streamwise natural transition
 - Gleyzes \rightarrow separation-induced transition
- 4-equation model:
 - Transport critical value of $Re_{\theta,cr}$
 - Integration/averaging of the Pohlhausen parameter Λ_2 following streamlines at BL edge
 - 2 x Integration of the curvilinear coordinate:
 - One for Λ_2 averaging
 - One for intermittency raising in the transition region

Stability-Based Transition Model using Transport Equations

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- Combination of two criteria on Re_θ :
 - AHD derived for streamwise natural transition $Re_{\theta,tr} = fn(Me, Tu, \bar{\Lambda}_2, Re_{\theta,cr})$
 - Gleyzes for separation-induced transition **Correction on $Re_{\theta,cr}$ when $Hi > 2.8$**
- 4-equation transition model:
 - Transport critical value of $Re_{\theta,cr}$ $Re_{\theta,cr} = fn(Me, Hi)$
 - Integration/averaging of the Pohlhausen parameter Λ_2 following streamlines at BL edge
 - 2 x Integration of the curvilinear coordinate:
 - One for Λ_2 averaging
 - One for intermittency raising in the transition region

**Relies on the
evaluation of BL
characteristics**

Stability-Based Transition Model using Transport Equations

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- Options

- Local Λ_2 can be derived either

- from wall pressure (**incompressible**)

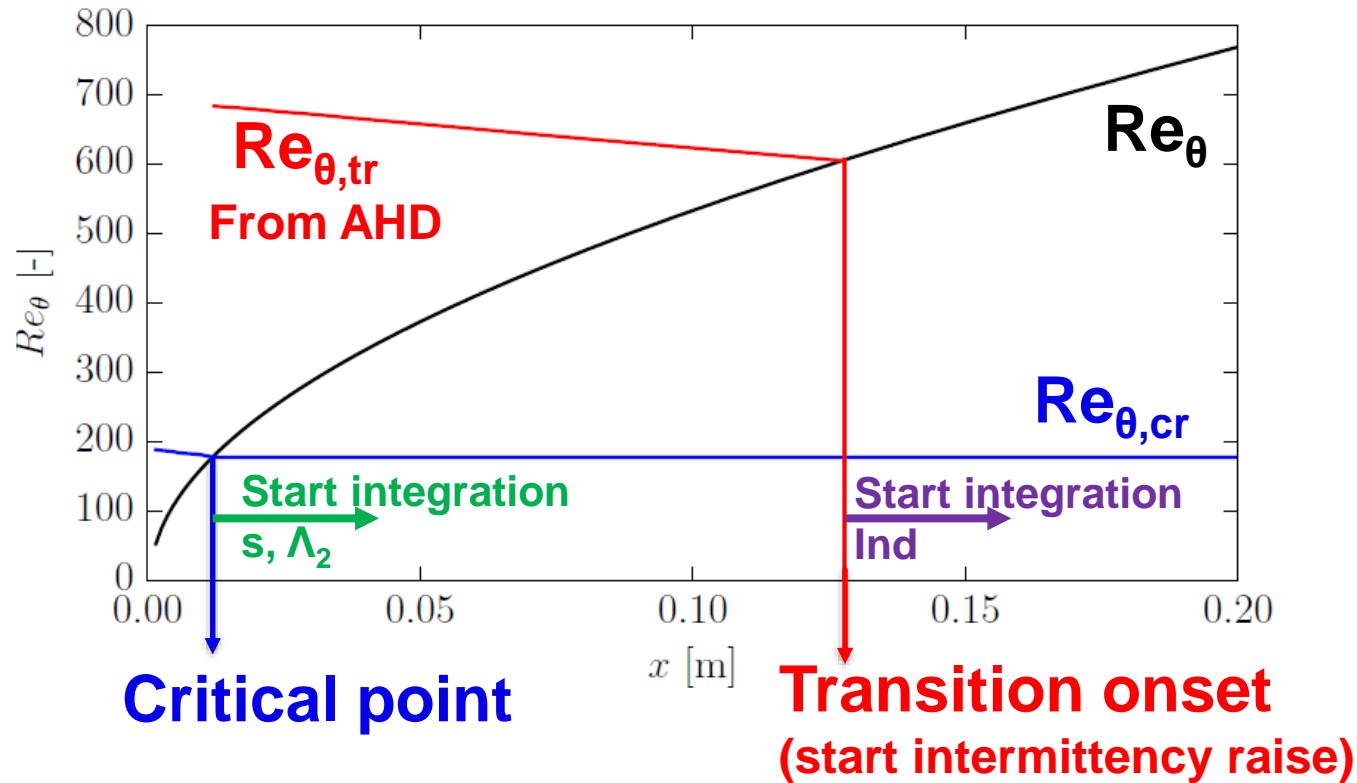
- • from BL edge velocity

- H_i can be either

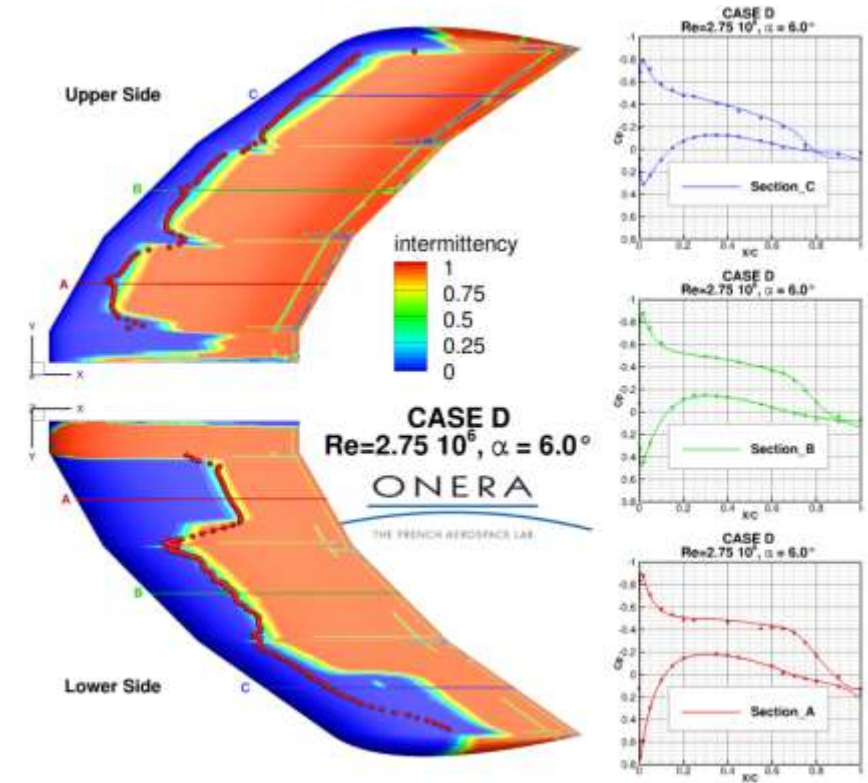
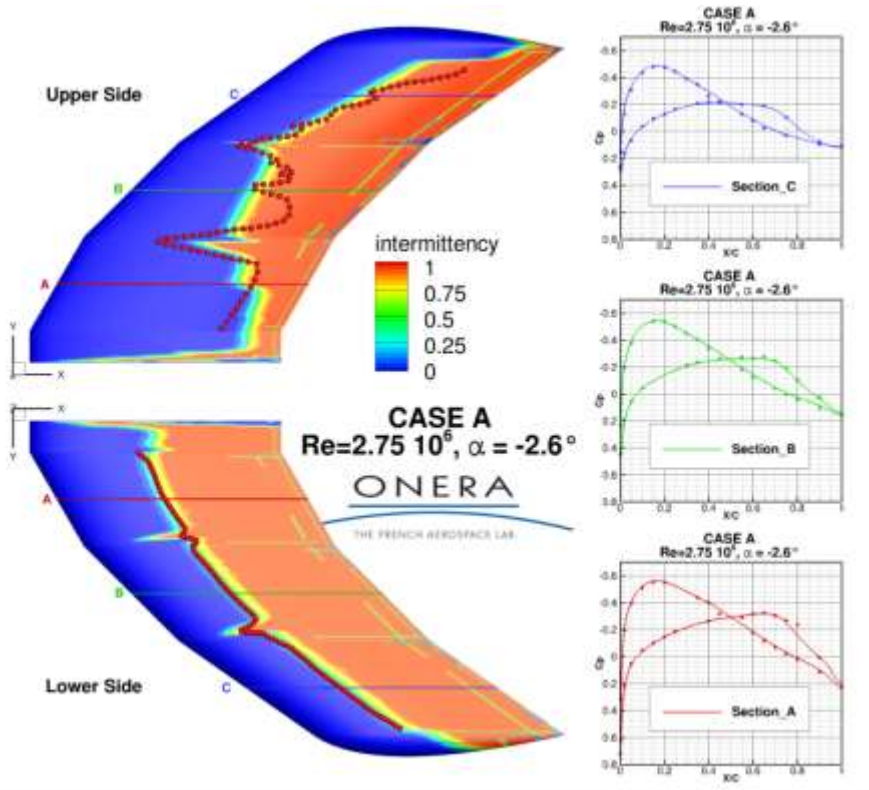
- • computed from BL profile integration (needs fine mesh for accurate results)

- from Λ_2 through correlation

Model behavior



Model behavior – Sickel Wing

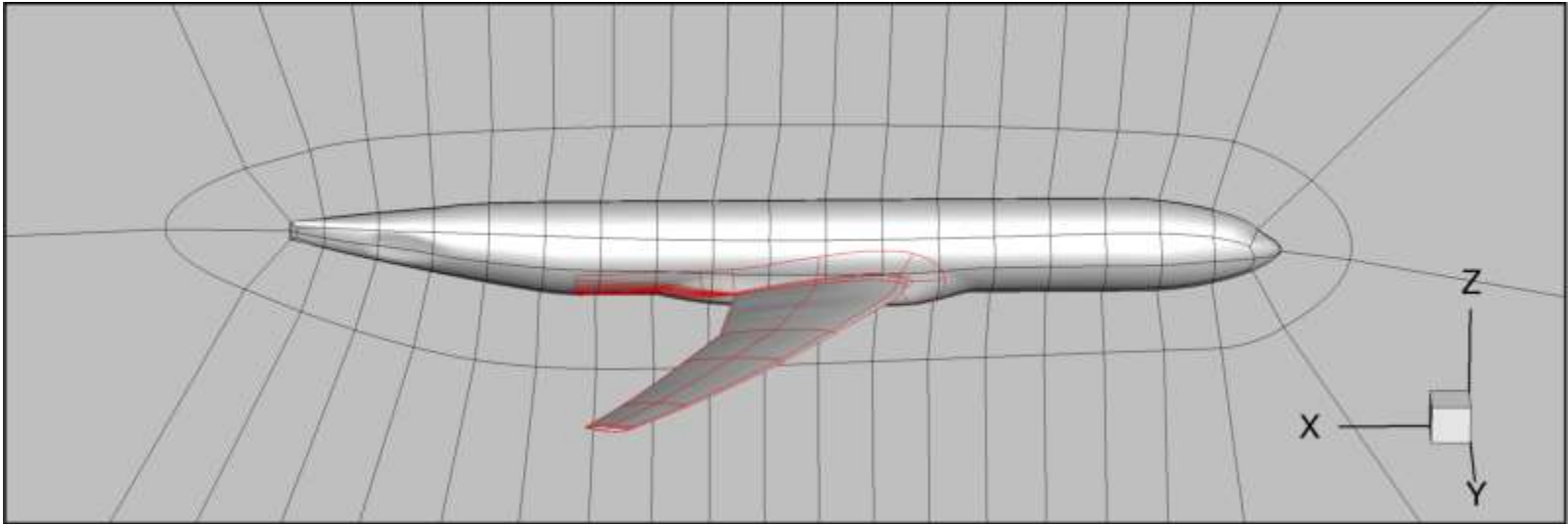


Outline

- Solver & models
- **Grids**
- Pressure coefficient, transition lines
- Force and moment data
- Perspectives

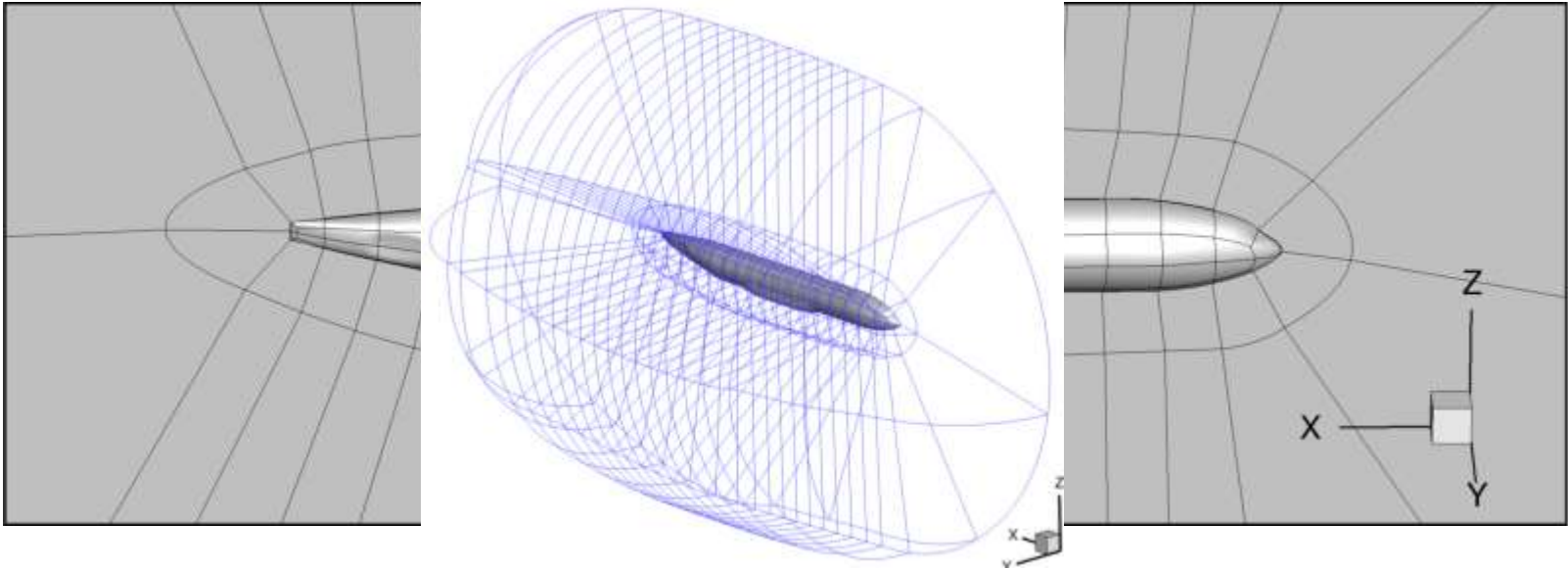
Grids

- Custom structured overset mesh



Grids

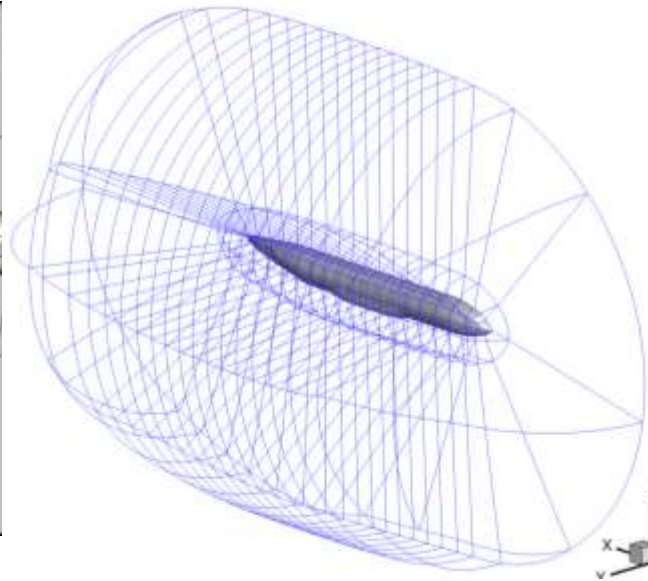
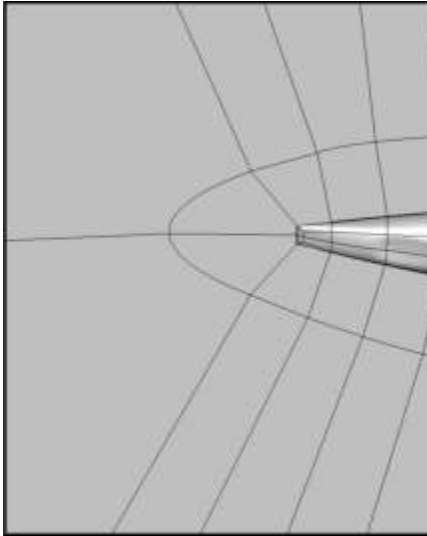
- Custom structured overset mesh



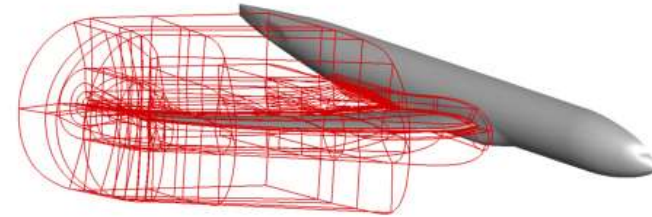
Fuselage nearbody

Grids

- Custom structured overset mesh



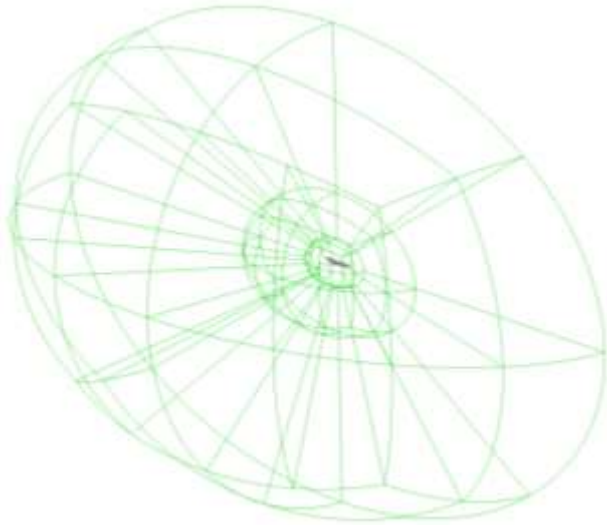
Fuselage nearbody



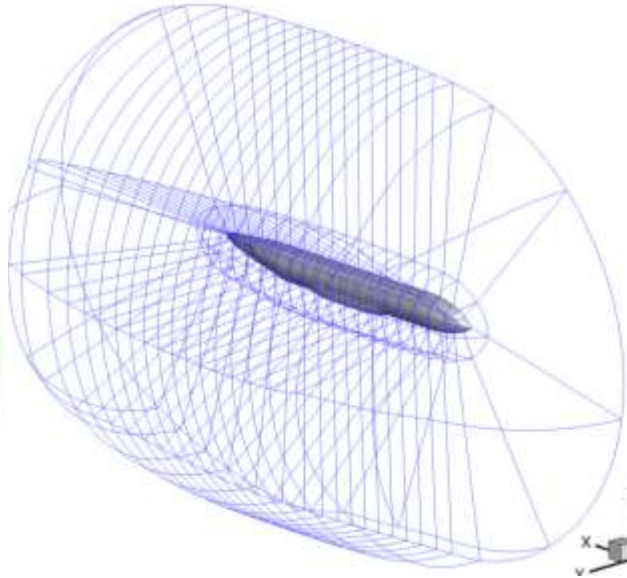
Wing C-mesh

Grids

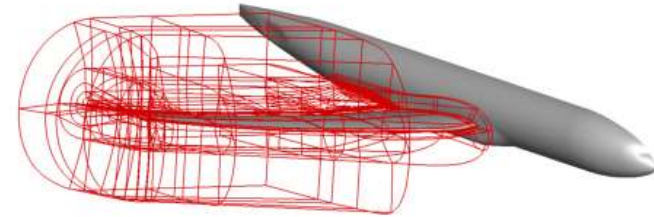
- Custom structured overset mesh



Background grid



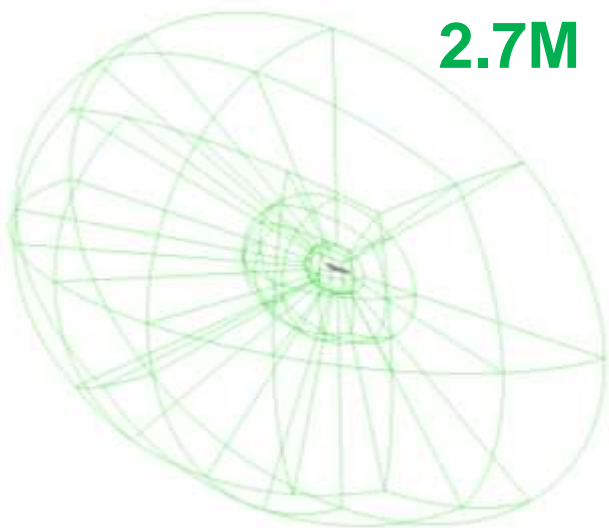
Fuselage nearbody



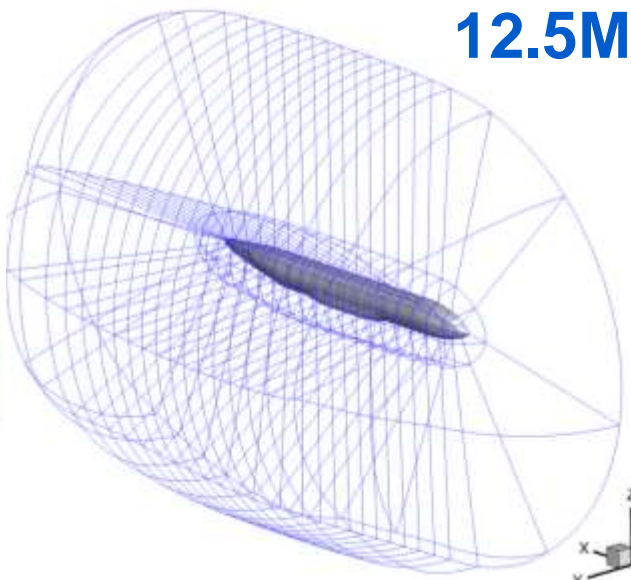
Wing C-mesh

Grids

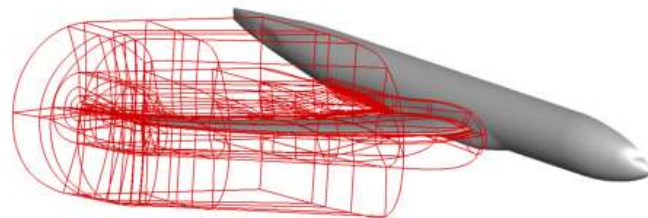
- Custom structured overset mesh (33.2M cells)



2.7M



12.5M



17.9M

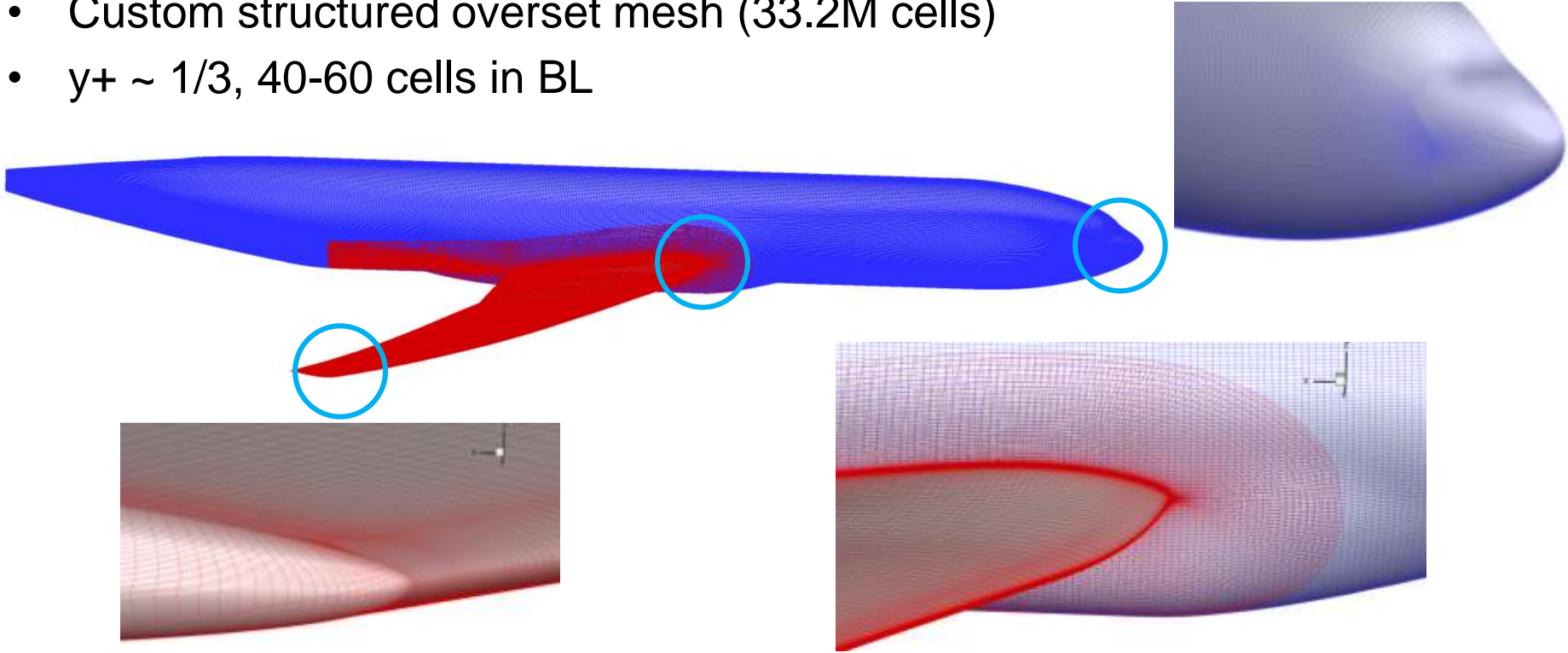
Background grid

Fuselage nearbody

Wing C-mesh

Grids

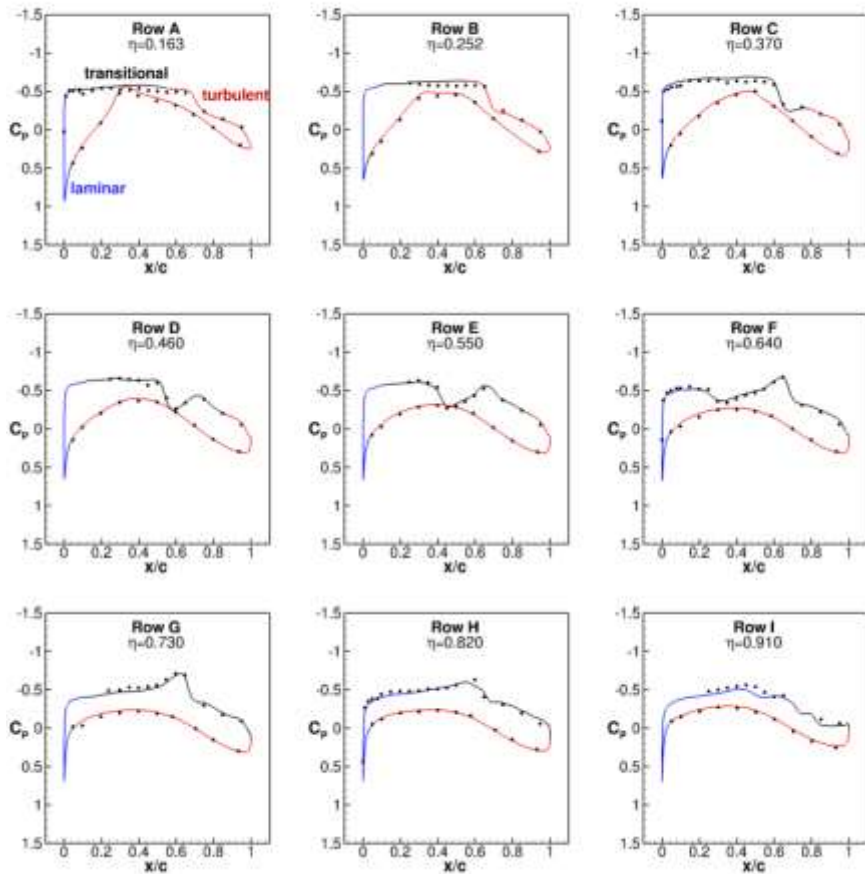
- Custom structured overset mesh (33.2M cells)
- $y^+ \sim 1/3$, 40-60 cells in BL



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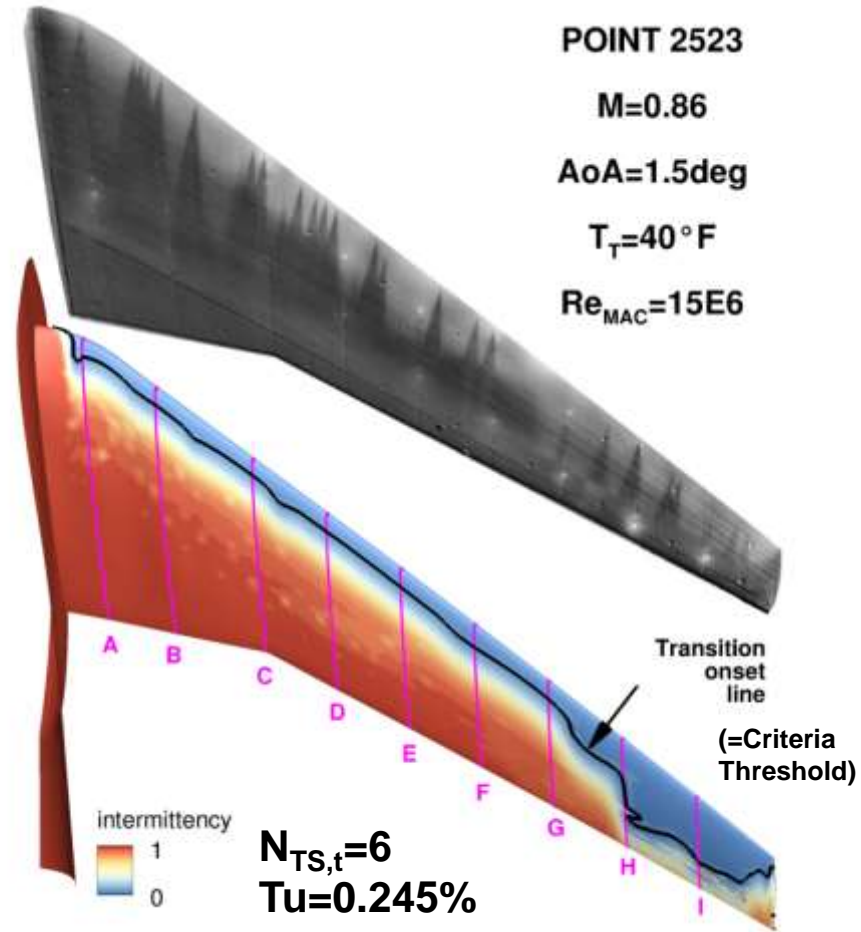
POINT 2523 M=0.86 AoA=1.5deg T_T=40°F Re_{MAC}=15E6



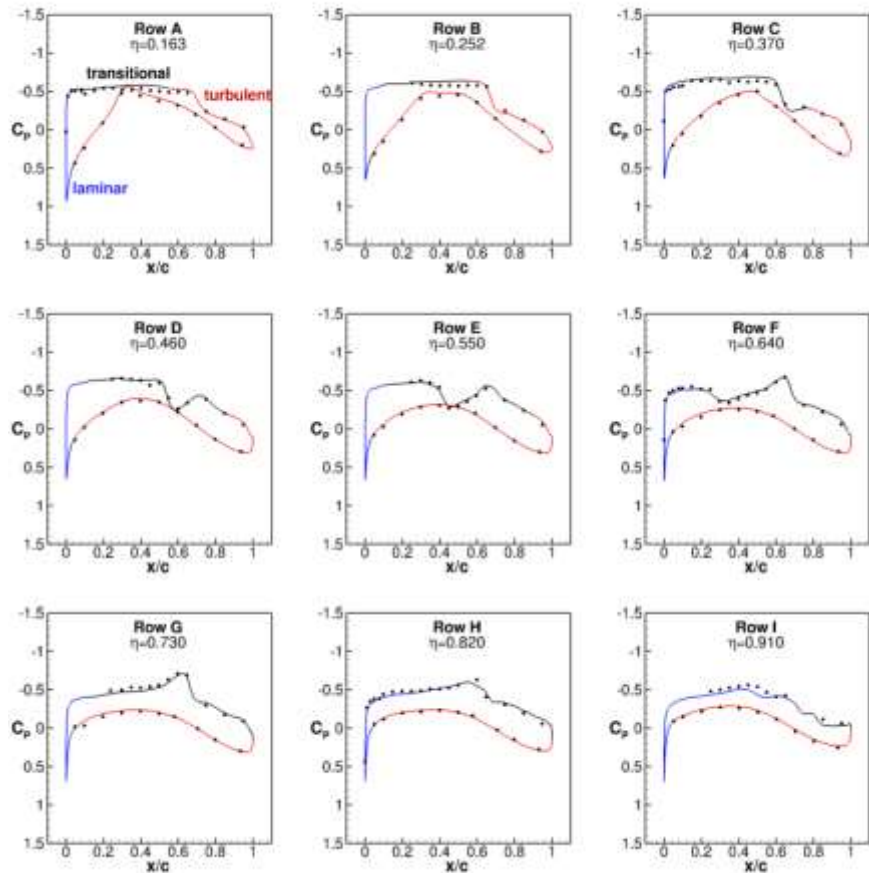
POINT 2523

M=0.86

AoA=1.5deg

 $T_T = 40^\circ \text{F}$
$$\text{Re}_{\text{MAC}} = 15\text{E}6$$


POINT 2523 $M=0.86$ $AoA=1.5deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$



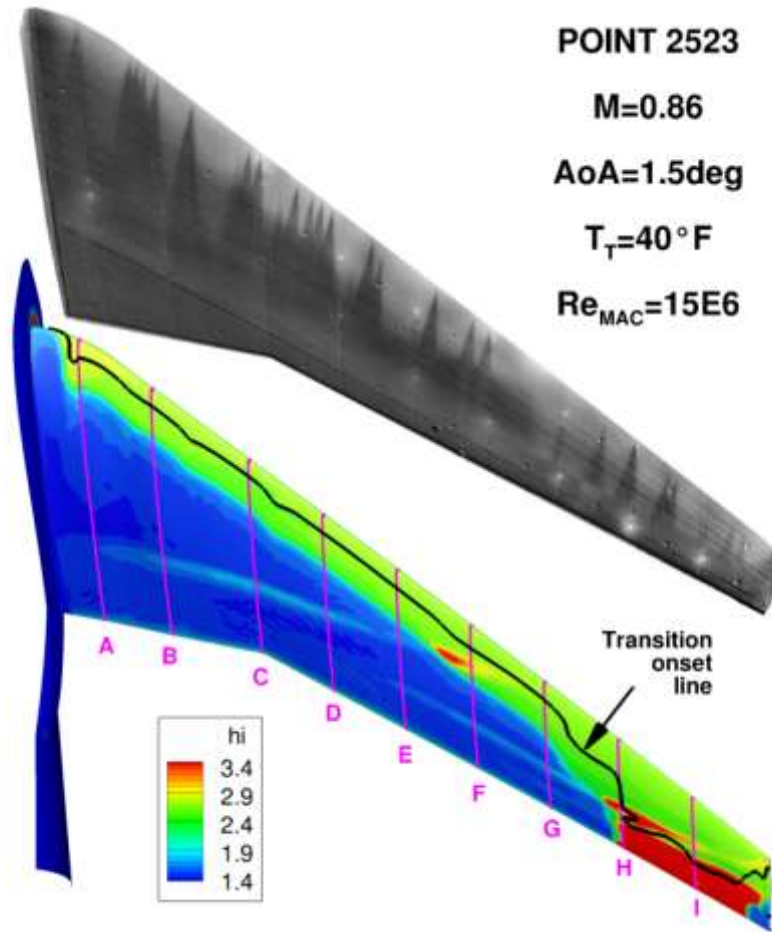
POINT 2523

$M=0.86$

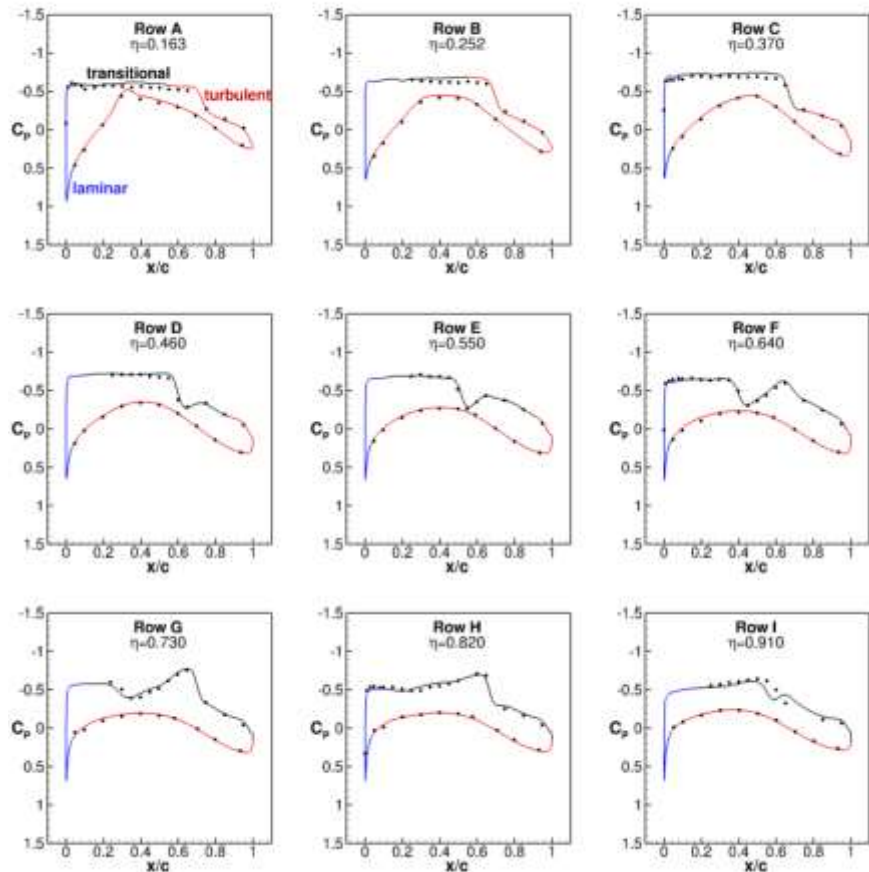
$AoA=1.5deg$

$T_T=40^\circ F$

$Re_{MAC}=15E6$



POINT 2524 $M=0.86$ $AoA=2.0deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$



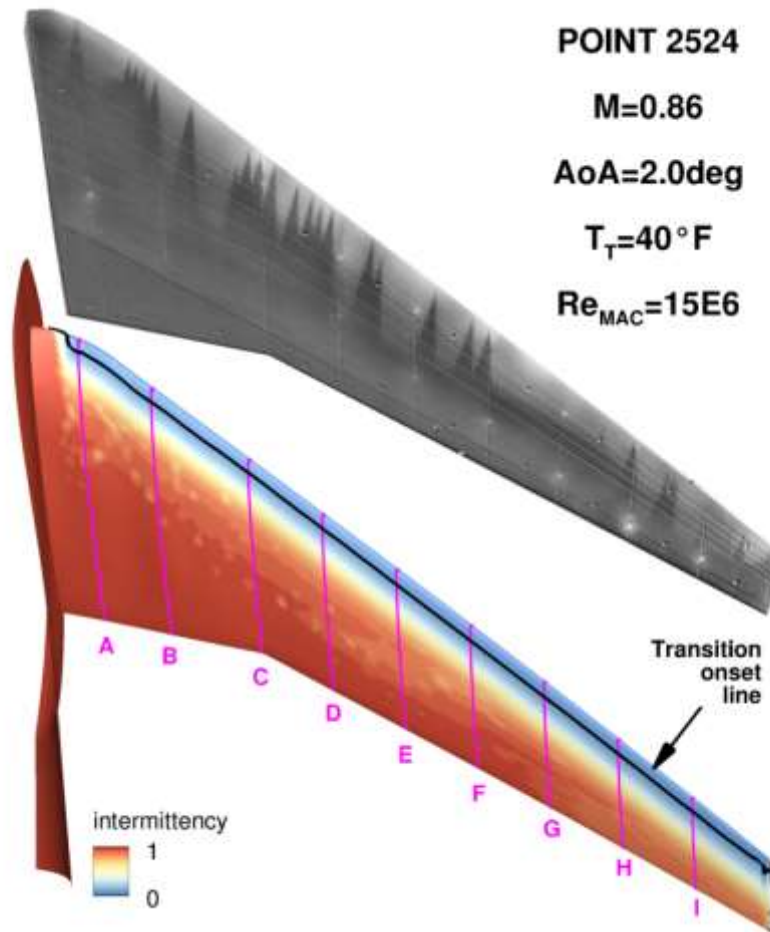
POINT 2524

$M=0.86$

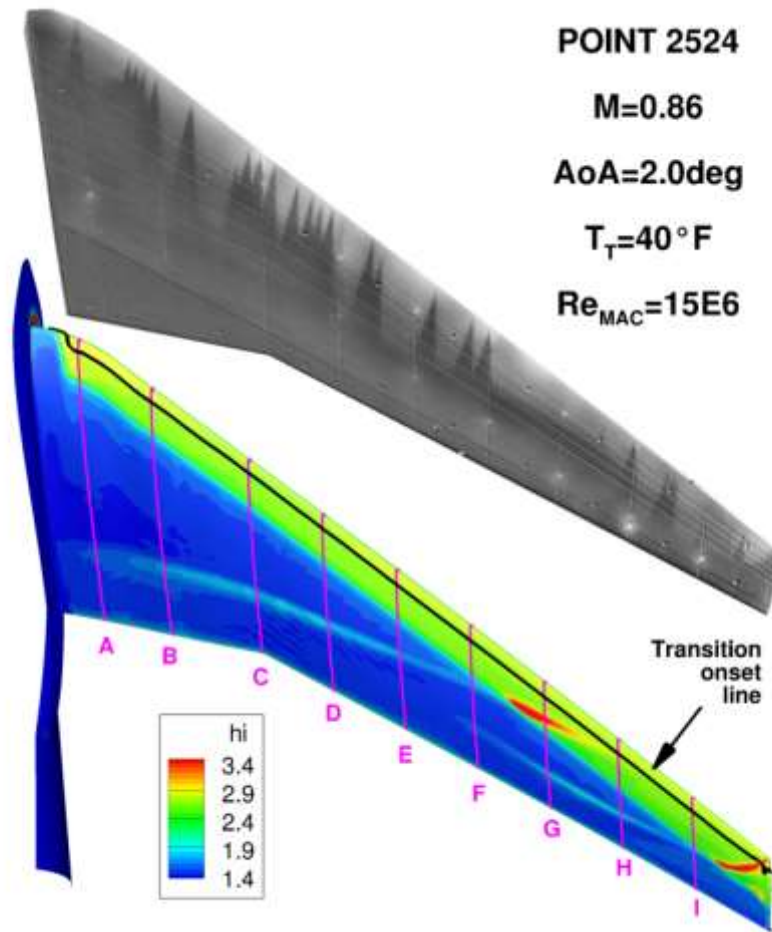
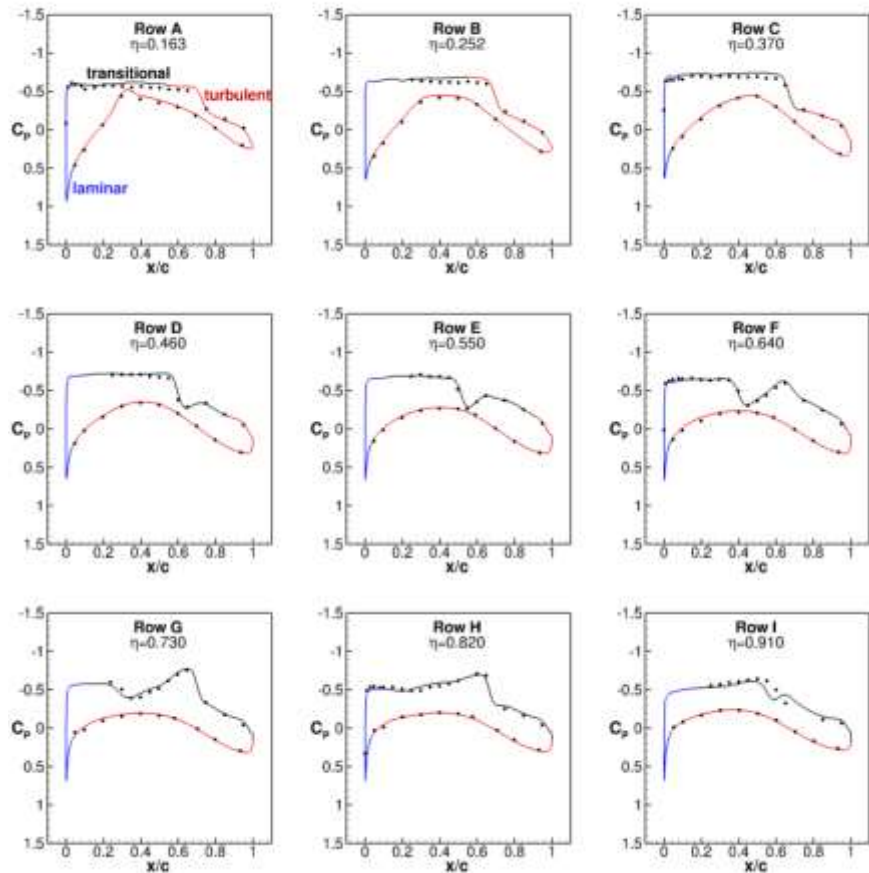
$AoA=2.0deg$

$T_T=40^\circ F$

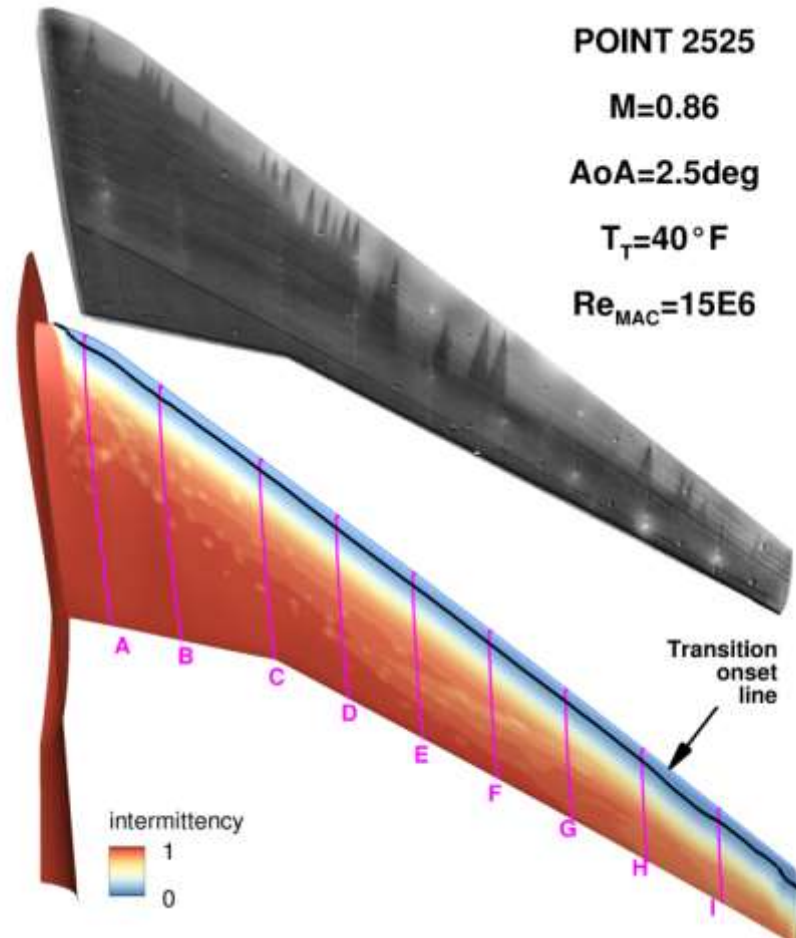
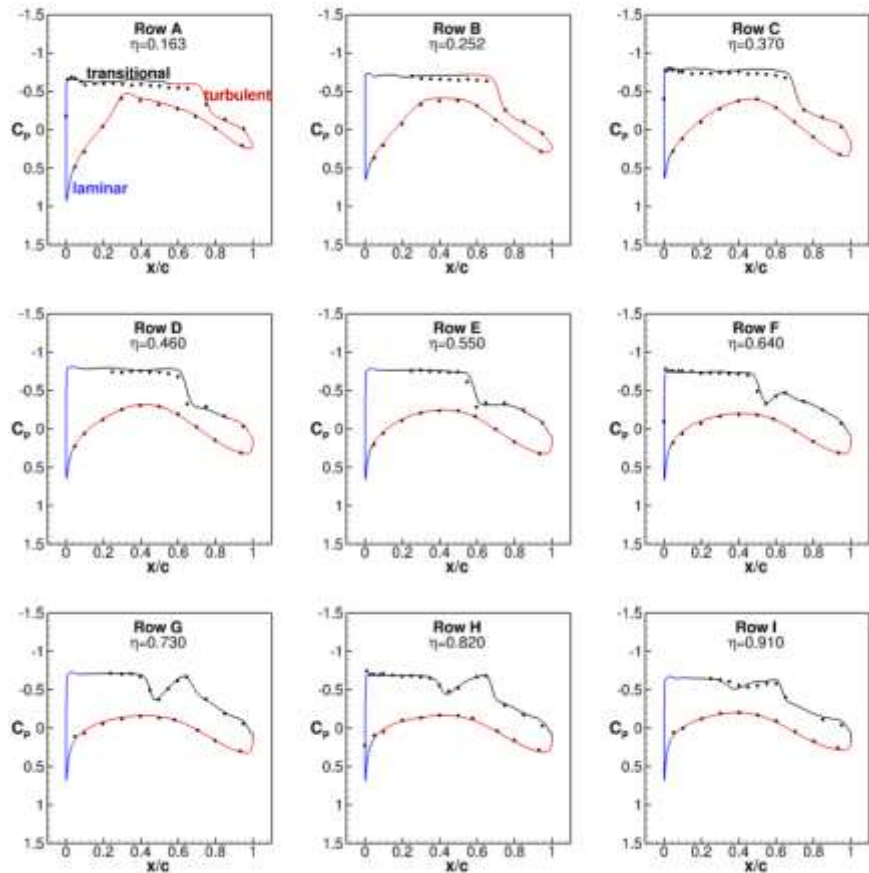
$Re_{MAC}=15E6$



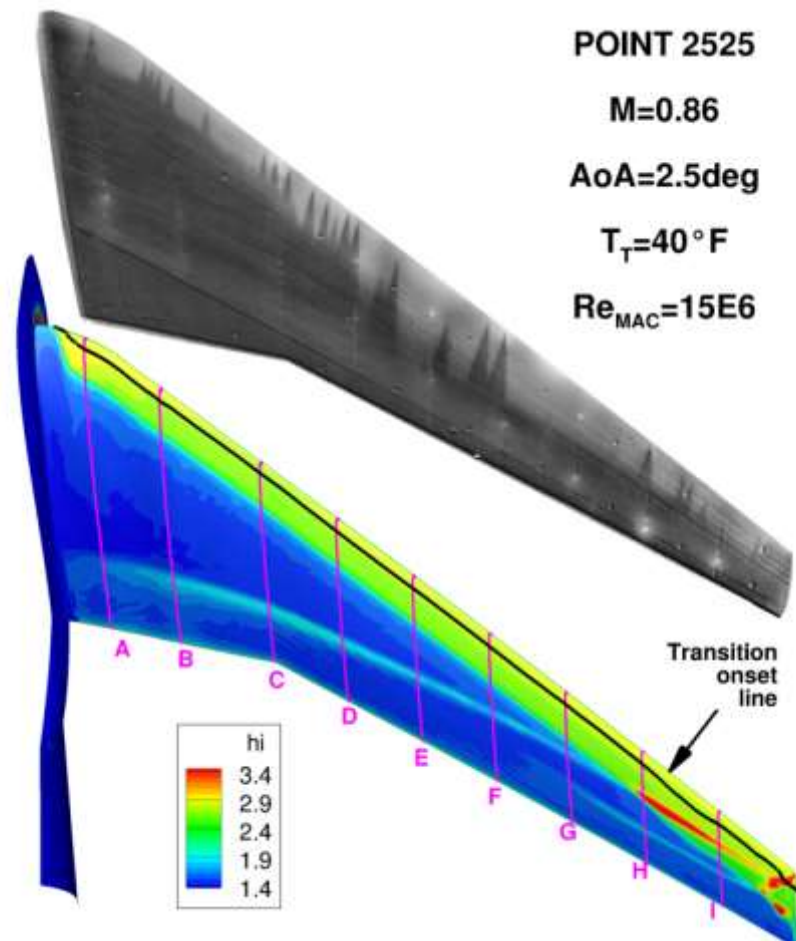
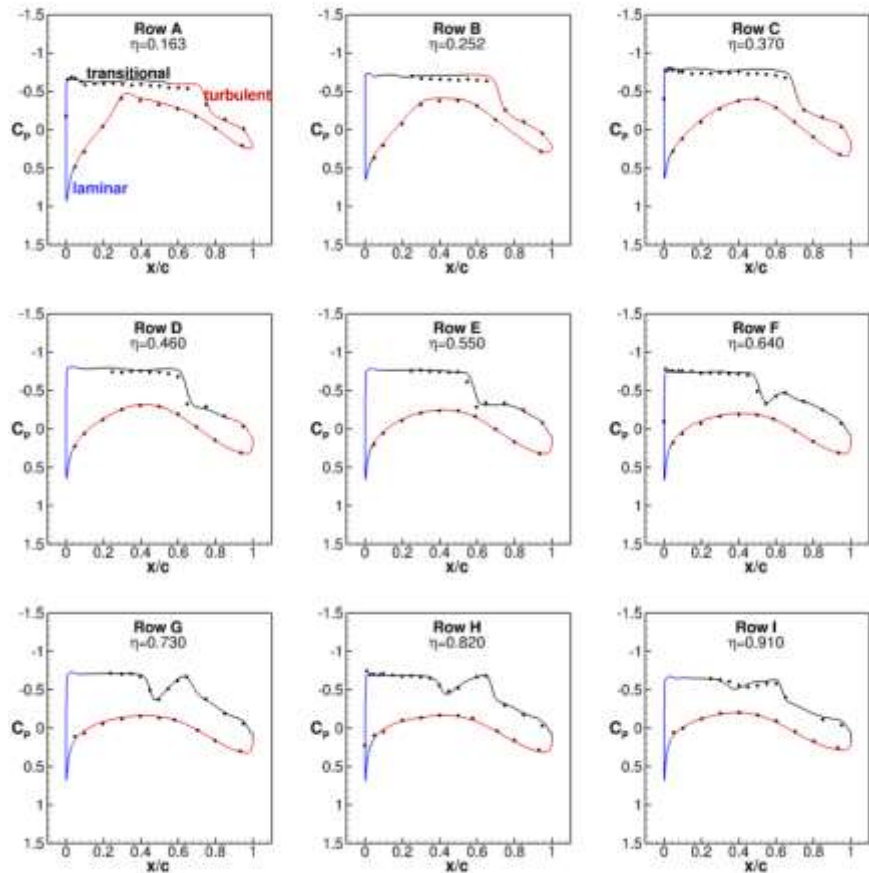
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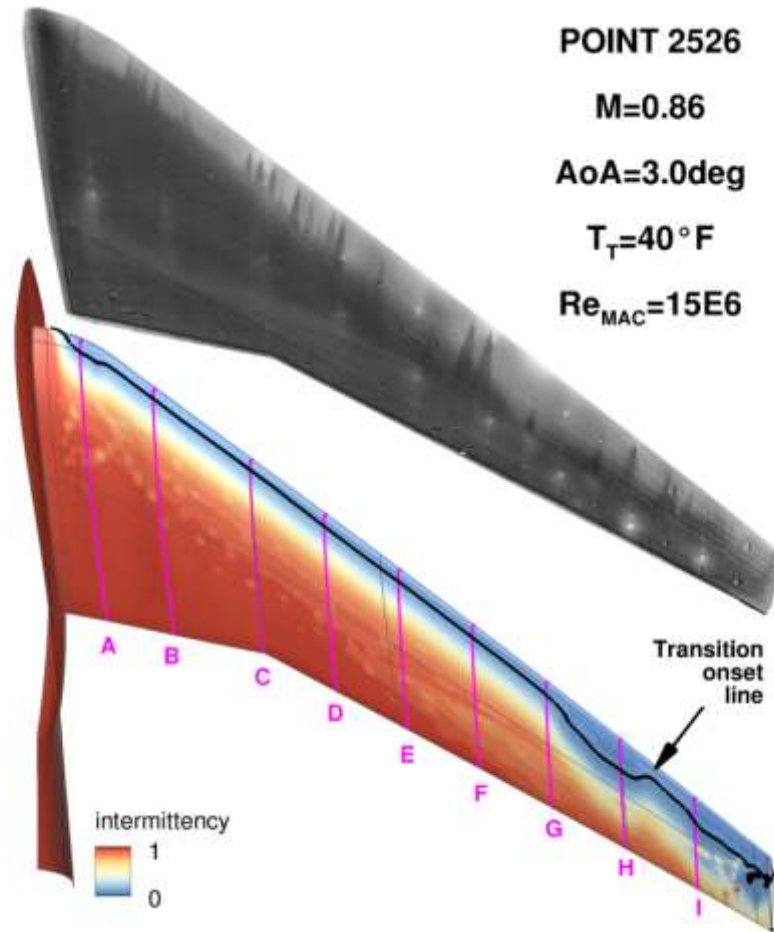
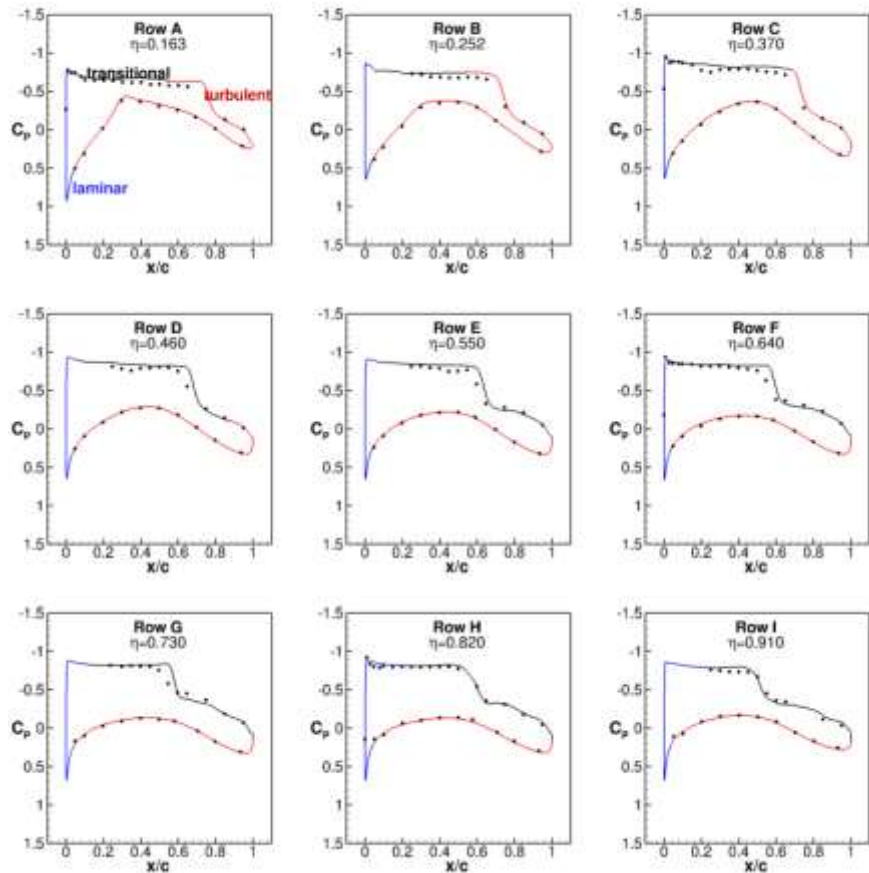
POINT 2525 $M=0.86$ $AoA=2.5deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$



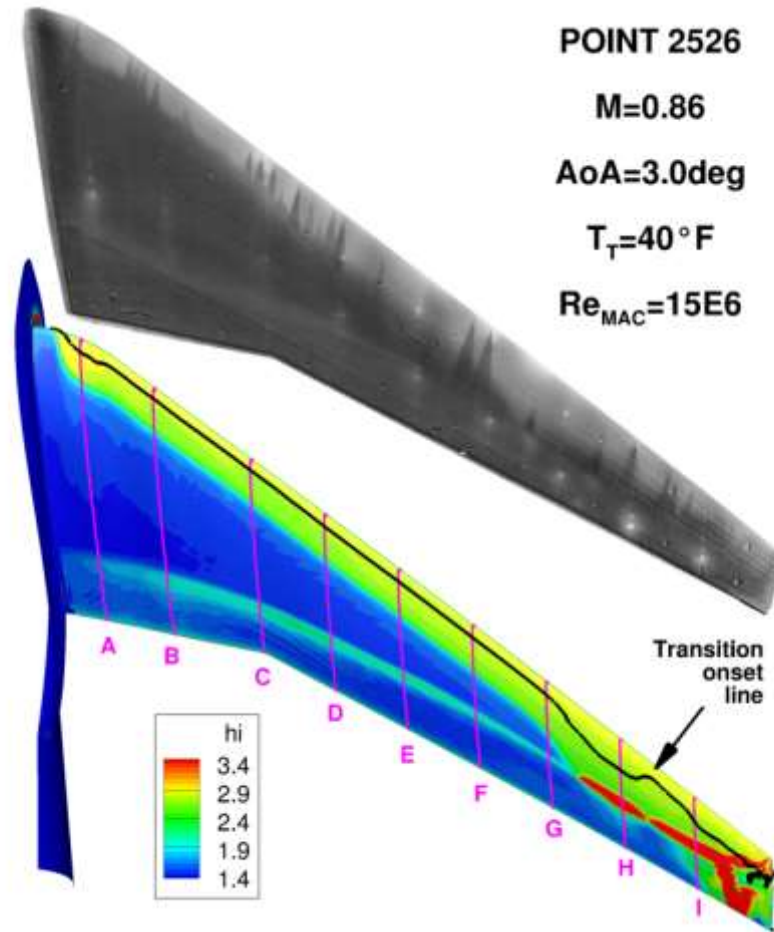
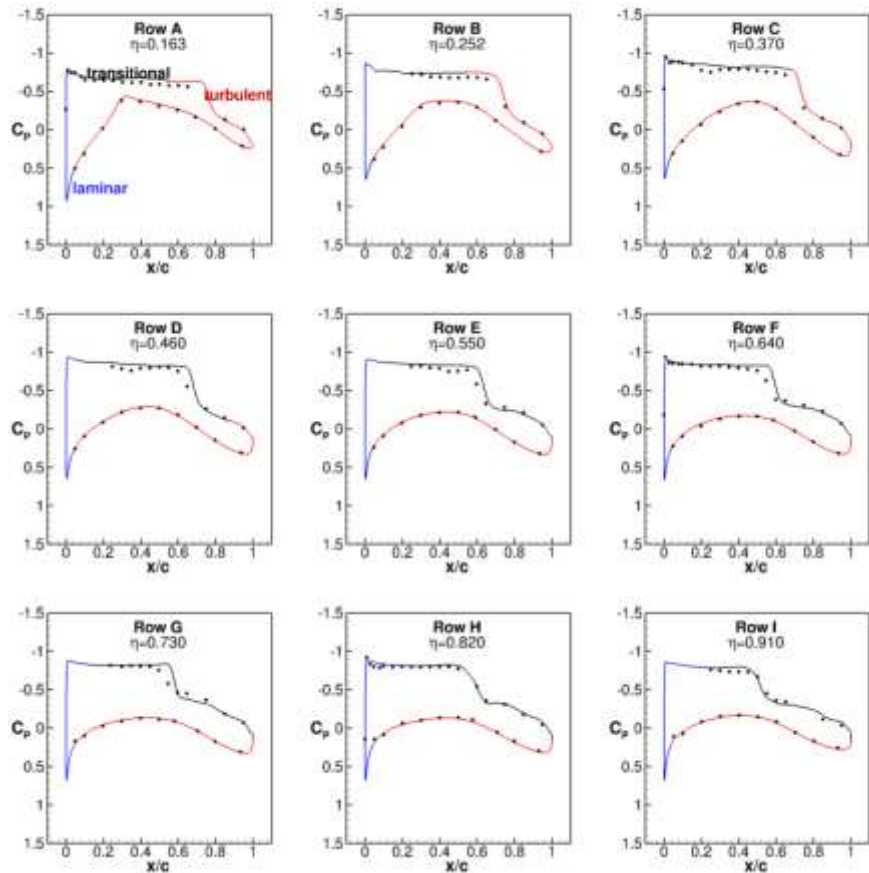
POINT 2525 $M=0.86$ $AoA=2.5deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$



POINT 2526 $M=0.86$ $AoA=3.0deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$

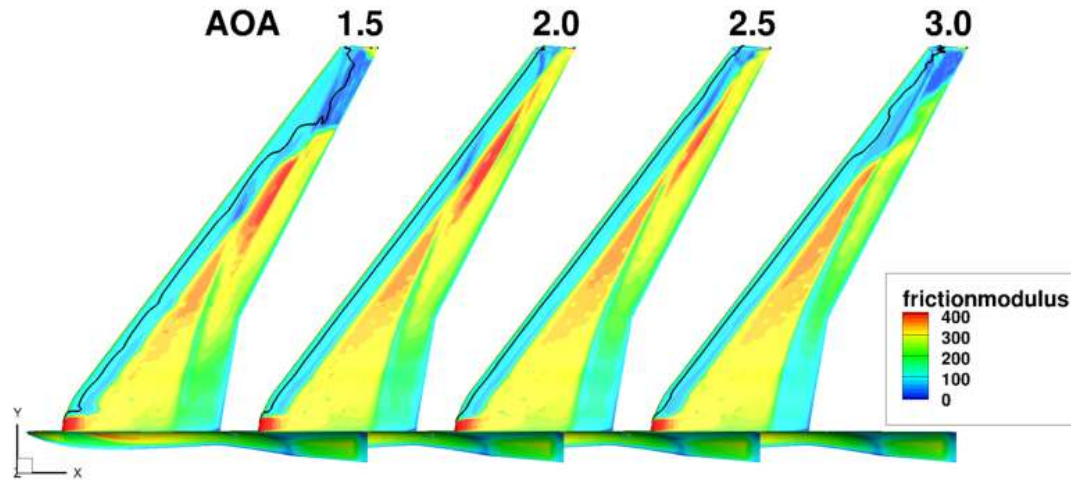


POINT 2526 $M=0.86$ $AoA=3.0deg$ $T_T=40^\circ F$ $Re_{MAC}=15E6$



Observations on CFD results

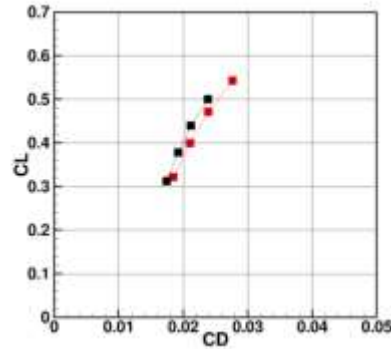
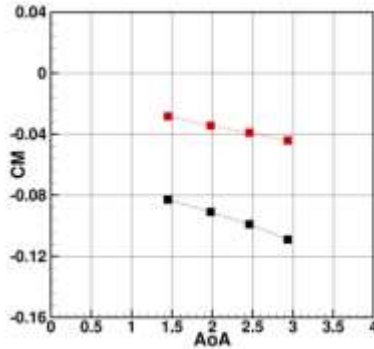
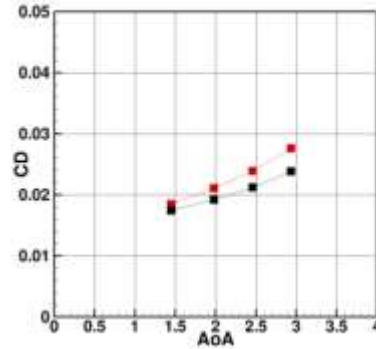
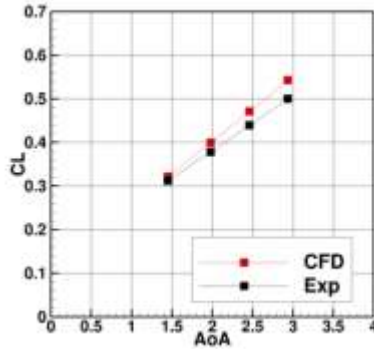
- AoA 1.5: shock-induced transition in the outboard region in the CFD
- Early transition locations due to criteria threshold reached near the elading edge, fixed transition length in the CFD probably too short.



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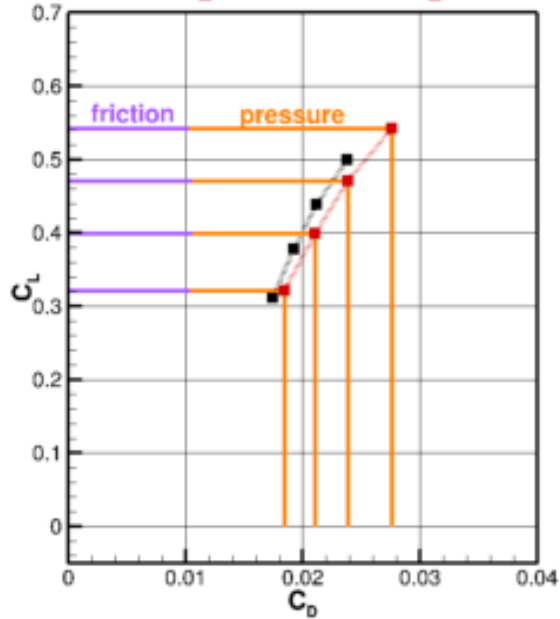
Force and moment data



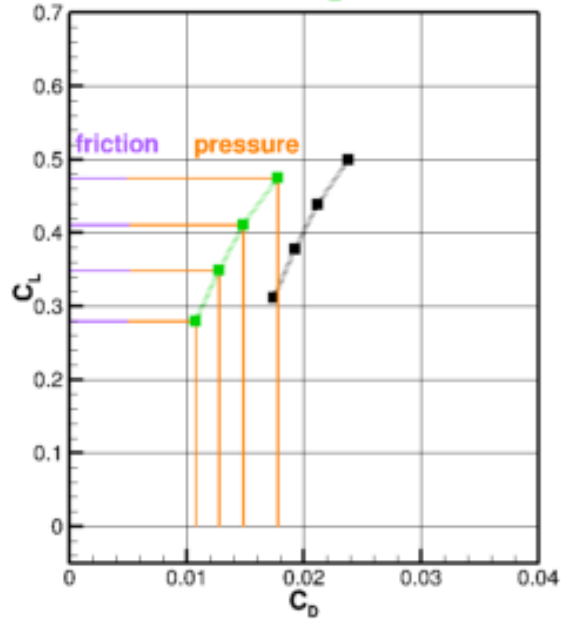
- Lift not too far from exp. values (recompression a little downstream of exp.)
- Drag overestimated (friction on wing)
- Pitching moment underestimated (Model Moment Center correct?)

Force breakdown

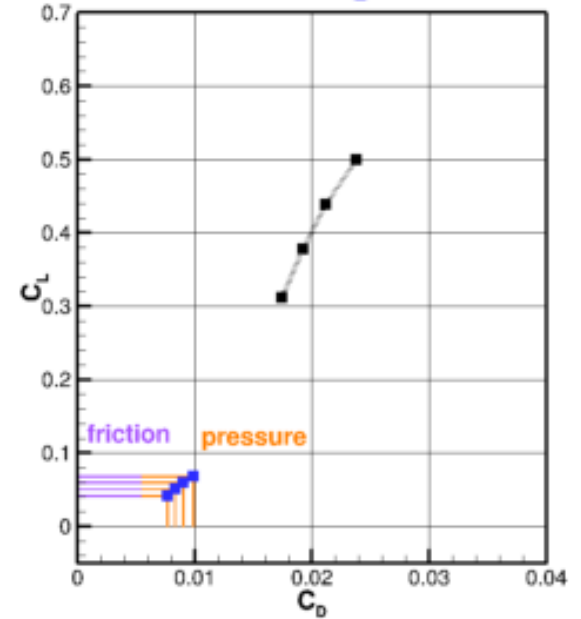
wing + fuselage



wing



fuselage



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Perspectives

- Investigate discrepancies on friction coefficient values (pressure side)
- Switch to new solver, ongoing validation for transition
- Will take a while, starting with simple test cases
- Grid convergence study in « full turbulent » on CRM-NLF using provided grids
(Current mesh smoothed out most of C_p chordwise oscillations)